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Equilibrium solubility of pure [and](http://www.elsevier.com/locate/tca) [mixed](http://www.elsevier.com/locate/tca) [3,5-dinitro](http://www.elsevier.com/locate/tca)benzoic acid and 3-nitrobenzoic acid in supercritical carbon dioxide

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ABSTRACT

The solid solubility of pure 3,5-dinitrobenzoic acid (3,5-DNBA) and 3-nitrobenzoic acid (m-NBA) and their equal-weight mixture in supercritical carbon dioxide $(SCCO₂)$ was measured using a flow-type apparatus at 308, 318, and 328 K and in the pressure range of 10.0–21.0 MPa. The solubility enhancement SE of mixed 3,5-DNBA and m-NBA in the ternary system has been observed. The mixture separation factor μ and the separation efficiency HE were investigated. A modified Kumar–Johnston (K–J) model was proposed for correlating the solubility of solid compounds in $SCCO₂$. The experimental solubility data of pure and mixed solutes in $SCCO₂$ were successful to be correlated by Chrastil model, the modified Adachi–Lu model, K–J model and new proposed model. Solubility data from 23 different solid compounds were taken from literature. The accuracy of the proposed model was evaluated by correlating 13 binary systems, 13 ternary systems, and 1 quaternary system. The modified K–J model satisfactorily correlated the experimental results for the solubility of all these compounds in SCCO₂ within 5.11% AARD.

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1. Introduction

Supercritical fluid (SCF) technology has gained a rapid growth for the past few decades, and has been widely applied in food processing, pharmaceutical industries, separation processes, chemical reaction and a variety of extractions [1]. Carbon dioxide $(CO₂)$ is a solvent of choice in SCF technology because it is inexpensive, nontoxic, readily available in relatively pure form, and has moderate critical constants (7.38 MPa and 304 K). Supercritical carbon dioxide ($SCCO₂$) has stro[ng so](#page-8-0)lvent power, high diffusivity and low viscosity. These unique properties make $SCCO₂$ an attractive solvent for many industrial separation and purification processes, especially in the pharmaceutical industry [2].

3,5-Dinitrobenzoic acid (3,5-DNBA) and 3-nitrobenzoic acid (m-NBA) are important pharmaceutical intermediate materials for the pharmaceutical industry. 3,5-DNBA is mainly used for the synthesis of sulfachrysoidine and the detection of ampicillin. m-NBA is used for the production of agricultu[ral](#page-8-0) [ch](#page-8-0)emicals and dyes, in particular for the synthesis of procaine hydrochloride, procaine ammonium salts, and amino-nitro benzoic acid. These two aromatic compounds are similar in production and application processes, and benzoic acid is their common raw material in industry [3]. It reports that benzoic acid reacts with a three mole ratio of the $BF_3 \cdot N_2O_5$ complex in carbon tetrachloride in 36 h at 70 ◦C to form 3,5-DNBA (70% yield) and m-NBA (9.3% yield). The mixture products of 3,5DNBA and m-NBA should be separated before further reaction and preparation of single pure compound. Thus, it is a necessary step to separate the mixture of 3,5-DNBA and m-NBA in industry.

For the separation and purification of pharmaceutical materials using $SCCO₂$ extraction technology, it is important to determine the solubility of solid compounds in SCCO₂. Many recent literature have reviewed the solubility data of solid compounds in $SCCO₂$ [4,5]. However, no solubility data of pure or mixed 3,5-DNBA and m-NBA in SCCO₂ have been listed in previous literature.

Because the experimental determination of the solubility of solid compounds in $SCCO₂$ at various temperatures and pressures is time consuming, modeling of the solubility [data](#page-8-0) [in](#page-8-0) $SCCO₂$ is essential. Models used for correlating the solubility data can be broadly classified as equation of state (EOS) based models and semi-empirical models [6,7]. EOS based models like cubic equation of state or perturbed equations need large and complicated computational methods and the knowledge of the solid properties (macroscopic critical properties and sublimation pressure are needed for cubic equations of state and molecular parameters for perturbed e[quation](#page-8-0)s). These data are normally not available for many complex pharmaceutical compounds, which are determined by group contribution methods [8,9]. Due to several drawbacks, an error is produced in their estimations.

On the other hand, semi-empirical equations, like density based models, only need available independent variables like pressure, temperature and density of pure SCF instead of solid properties. They are based on si[mple](#page-8-0) [e](#page-8-0)rror minimization. The only drawback is the semi-empirical character, which means that solubility data are needed [10]. Recently, many semi-empirical models such as

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Table 1

 a T_m is the melting point of compound searching from the website of Chem YQ.

Chrastil model [11], Méndez-Santiago and Teja model [12], Bartle model [13], Gordillo model [14], del Valle and Aguilera model [15], Adachi and Lu model [16], Sparks model [17], Kumar and Johnston (K–J) model [18], and Yu model [19] are used for correlating the solu[bility](#page-9-0) data of solid compounds in $SCCO₂$. However, it is still uncertain which is the best model to predict more accurately for the [so](#page-9-0)lubility [data of](#page-9-0) [solid](#page-9-0) solutes in $SCCO₂$, especially [for](#page-9-0) [the](#page-9-0) mixtures of solid solutes.

[Thus](#page-9-0), an excellent [mathe](#page-9-0)matical modeling of solubility data in SCF could provide better understanding of the dissolution phenomenon and can be used for solubility prediction at interested pressures and temperatures after measuring a minimum number of experimental data, which could speed up the development of SCF technology.

In this work, the solubility of pure and mixed 3,5-DNBA and m -NBA in SCCO₂ was measured at 308, 318, and 328K over a pressure range from 10.0 to 21.0 MPa. The optimal operation for the separation of 3,5-DNBA and m -NBA using $SCCO₂$ extraction technology was investigated. The experimental solubility data were correlated by Chrastil model, the modified Adachi and Lu model, and K–J model. A modified semi-empirical model with four parameters based on K–J model was developed and used to correlate the solubility data of 25 different solid compounds from this work and literature.

2. Experimental methods

2.1. Chemicals and raw materials

Carbon dioxide (CAS 124-38-9) (more than 99.9% mass fraction) was purchased from Beijing Praxair Industrial Gas Co., Ltd. 3,5-DNBA ($C_7H_4N_2O_6$, CAS 99-34-3) and m-NBA ($C_7H_5NO_4$, CAS 121-92-6) with an assessed minimum mass purity of 99% (analytical purity) were purchased from Beijing Hengye Zhongyuan Chemical Co., Ltd. The chemical structures and melting points of solid compounds are shown in Table 1. All chemicals were used without further purification.

2.2. Experimental procedure

The solubility of 3,5-DNBA and m -NBA in SCCO₂ was measured using a dynamic flow technique with ultraviolet spectrophotometer analysis. A schematic diagram of the experimental apparatus is shown in Fig. 1.

 $CO₂$ supplied to a high-pressure surge flask from a cylinder was pressurized by the compressor (Nova, model 5542121). Highpressured $CO₂$ entered into a preheating and mixing cell with a heating electric coil so that its temperature and pressure could reach to the operating condition. $SCCO₂$ entered into a highpressure equilibrium cell with an available volume of 150 mL from the bottom consecutively, which was loaded 40 or 50 g of packed solute mixed with the glass beads and stainless steel sintered disks at both ends to prevent physical entrainment of undissolved solute. The high-pressure equilibrium cell was immersed in a constanttemperature stirred water bath with preheating coils (Chongqing Yinhe Experimental Instrument Corporation, model CS-530), which was controlled to ± 0.5 K by a temperature controller. The temperature and pressure in the cell was measured by a calibrated internal platinum resistance thermometer (Beijing Chaoyang Automatic Instrument Factory, model, XMT) and a calibrated pressure gauge (Heise, model CTUSA), respectively. The uncertainty for temperature measurement is \pm 0.1 K, and that for pressure is \pm 0.05 MPa.

Fig. 1. Schematic diagram of the experimental apparatus: 1, CO₂ cylinder; 2, compressor; 3, high-pressure surge flask; 4, pressure regulating valve; 5, preheating and mixing cell; 6, high-pressure equilibrium cell; 7, decompression sampling valve; 8, U-shaped tube;9, rotated flow meter; 10, wet-gas flow meter;11, back pressure valve; 12, safety valve; 13, pressure gauge; 14, constant-temperature stirred water bath; 15, preheating coils; 16, temperature controller; 17, thermometer; 18, heating coils.

 $SCCO₂$ flowed out from the top of the equilibrium cell through a decompression sampling valve (wrapped with heating coils) and the solid compound was separated from $CO₂$ and collected by two U-shaped tubes in turn. From experimental observation, nearly all the solute was collected in the first U-shaped tube, and scarcely little precipitated in the second U-shaped tube. 3,5-DNBA is hardly soluble in water and very soluble in ethanol, while m-NBA is both soluble in water or ethanol. As a result, the solvent used to wash the analytes in the U-shaped tubes was the mixed solvent of ethanol and water (the volume ratio of ethanol and water = 1:3). The total volume of $CO₂$ released during the experiment was measured by a calibrated wet gas flow meter (Changchun Instrument Factory, model LML-2) with an uncertainty of ± 0.01 L at room temperature and atmospheric pressure.

To make sure the reliability of the experimental procedure, the equilibrium time and the suitable flow rate of $CO₂$ was determined, respectively. The flow rate experiments with a rotated flow meter were carried out before. The results showed that when the flow rate of CO_2 was in the range of 0.3–1.0 L min⁻¹, the equilibrium of system would be maintained. The average flow rate of 0.6 L min−¹ in this work was adopted. At a suitable flow rate of CO2, the solubility of solutes was measured after 20, 30, 40, 50, and 60 min, respectively. The results showed that the solubility was nearly invariable after 30 min, which shows that the system had reached equilibrium. Therefore, all of the data were measured after 30 min.

2.3. Analytical methods and solubility measurements

UV spectrophotometer (UNICO, model UV-2100) method was used to analyze the amount of solutes collected in the U-shaped tubes. The reference solution was the mixed solvent of ethanol and water (the volume ratio of ethanol and water = 1:3). The maximum UV absorption λ_{max} of the sample was detected at a wavelength of 263 nm for 3,5-DNBA and 268 nm for m-NBA, respectively. A calibration curve was used to establish the concentration of solute with the regression coefficient better than 0.9995. The solubility of solute was determined by the concentration of solute and the flow volume of $SCCO₂$, and the solubility of solute in mole fraction was calculated according to the following formula:

$$
y = \frac{S \times M_1}{S \times M_1 + \rho \times M_2}
$$
 (1)

where S is the solubility of solute (g L⁻¹), M_1 and M_2 are the molecular weights of CO₂ and solute (gmol⁻¹), respectively, ρ is the density of $CO₂$ at room temperature and normal atmospheric pressure (gL^{-1}), and y is the mole fraction solubility of the solute.

For the solubility measurements of mixed 3,5-DNBA and m-NBA in $SCCO₂$, the cumulative absorbance was resulted from the comprehensive contribution of both 3,5-DNBA and m-NBA. Thus, each composition of solutes in the ternary system (3,5-DNBA + m- $NBA + SCCO₂$) was determined by an absorbency measurement at both wavelengths of 268 nm (the maximum wavelength of m-NBA) and 237 nm (obtained by detecting the wavelength to acquire a maximum absorption difference with the absorption at 268 nm) using UV spectrophotometer. Consequently, the solubility of each solute was calculated by a least-squares regression from the relative absorbency at both wavelengths.

The reliability of the experimental apparatus was verified by measuring the solubility of solid solutes in our previous work [20,21]. Each reported data point in this work was the average of at least three replicated sample measurement to ensure the accuracy. The uncertainty of each measurement was within ± 5 %.

3. Theoretical section

3.1. Empirical models

Chrastil model [11] is one of the most frequently used densitybased models, which indicates that the relationship between the solute solubility (S, gL⁻¹) in SCF and the solvent density (ρ_1 , gL⁻¹) and temperature (T, K) as:

$$
\ln S = A_0 \ln \rho_1 + \frac{A_1}{T} + A_2 \tag{2}
$$

where A_0 – A_2 are the model constants that can be estimated from experimental solubility data in SCF. A_0 is an association constant describes the number of SCF molecules in the solvated complex, A_1 is a function of the enthalpy of salvation and vaporization, and A_2 is a function of the association number and molecular weights of the solute and SCF.

Adachi and Lu [16] modified Chrastil's model to better model the solubility of triglycerides. Chrastil assumed the association number A_0 to be constant and independent of density. Adachi and Lu changed the association number A_0 to a second-order polynomial of density. They proposed that the association constant A_0 could be expre[ssed](#page-9-0) [a](#page-9-0)s $A_0 = e_0 + e_1 \rho_1 + e_2 \rho_1^2$. They found that a significant reduction in variation between experimental and calculated solubility data could be achieved for some systems by modifying the association number A_0 .

Sparks et al. [17] found that Adachi and Lu modified the term for the association constant A_0 in Chrastil model so that it became a quadratic function of density. However, when values of the modified A_0 were calculated for several solid-SCCO₂ systems [16] and plotted against reduced density, an interesting trend can be obse[rved.](#page-9-0) Though A_0 was generated from a quadratic function, the change of A_0 with density is somewhat linear for each compound. Therefore, Adachi and Lu model can be s[implifi](#page-9-0)ed (with insignificant loss of efficacy) to the following form as $A_0 = e_0 + e_1 \rho_1$. Therefore, the solubility of solute (S, gL^{-1}) in SCF can be correlated to the solvent density (ρ_1 , gL⁻¹) and temperature (T, K) by the modified Adachi and Lu model:

$$
\ln S = (B_0 + B_1 \rho_1) \ln \rho_1 + \frac{B_2}{T} + B_3 \tag{3}
$$

where $B_0 - B_3$ are the model constants.

Kumar and Johnston [18] pointed out that the linear relationships observed between $\ln y_2$ and $\ln \rho_1$ and in some cases between $\ln y_2$ and ρ_1 are system dependent and neither can be validly generalized. Similar to Eq. (2), the linear expression between $\ln y_2$ and ρ_1 could be g[iven a](#page-9-0)s:

$$
\ln y_2 = C_0 \rho_1 + \frac{C_1}{T} + C_2 \tag{4}
$$

where y_2 is the mole fraction solubility of solute in SCF, ρ_1 (g L⁻¹) is the solvent density, $T(K)$ is temperature, and C_0-C_2 are the model constants.

K–J model is expressed with three adjustable parameters $(C_0,$ C_1 and C_2) in Eq. (4). The value of C_1 is related to the total heat ΔH_{total} (heat of solvation ΔH_{sol} , plus heat of vaporization of the solute $\Delta H_{\rm vap}$), which cannot be changed random in the experiment. Parameter C_2 is a constant only acquired from the experimental data. Take into account the viewpoints of Adachi and Lu and Sparks et al. [16,17], the adjustable parameter C_0 should be related with density. Thus, C_0 is defined in this work as $C_0 = D_0 + D_1 \ln \rho_1$, which is linear with $\ln \rho_1$, rather than a constant, as K–J model simulated.

The following empirical model was proposed for the solubility [of s](#page-9-0)olid solutes in SCF as:

$$
\ln y_2 = (D_0 + D_1 \ln \rho_1)\rho_1 + \frac{D_2}{T} + D_3 \tag{5}
$$

Table 2 The mole fraction solubility of pure (y_b) and mixed (y_t) 3,5-DNBA and m-NBA in SCCO₂ with the solubility enhancement SE, mixture separation factor μ and the separation efficiency HE at temperatures of 308, 318, and 328 K and a pressure range of 10.0–21.0 MPa.

T(K)	p(MPa)	ρ_1 ^a (g/L)	3,5-DNBA			m -NBA			μ	HE $(\%)$
			$10^6 \cdot y_b$	$10^6 \cdot y_t$	SE(%)	$10^6 \cdot y_{\rm b}$	$10^6 \cdot y_t$	SE(%)		
308	10.0	714.84	0.58	1.22	110	7.21	7.43	3	6.09	85.90
	12.0	768.42	0.73	2.27	211	14.32	16.85	18	7.42	88.13
	15.0	816.06	0.94	2.69	186	19.44	27.56	42	10.25	91.11
	18.0	848.87	1.08	3.12	189	24.08	33.55	39	10.75	91.49
	21.0	874.40	1.09	3.45	217	25.36	37.71	49	10.93	91.62
			Average		183			30	9.09	89.65
318	10.0	502.57	0.48	0.51	6	3.33	4.43	33	8.69	89.68
	12.0	659.73	1.17	2.45	109	14.94	22.92	53	9.36	90.34
	15.0	743.17	1.69	3.86	128	34.34	40.68	18	10.54	91.33
	18.0	790.18	2.14	5.09	138	47.03	62.60	33	12.30	92.48
	21.0	823.71	2.30	7.11	209	60.68	74.61	23	10.49	91.30
			Average		118			32	10.27	91.03
328	10.0	326.40	0.44	0.45	$\overline{2}$	1.44	1.71	19	3.80	79.17
	12.0	506.85	1.31	1.50	15	10.38	12.02	16	8.01	88.91
	15.0	654.94	2.65	4.89	85	46.19	56.08	21	11.47	91.98
	18.0	724.13	3.57	7.23	103	79.59	90.02	13	12.45	92.57
	21.0	768.74	4.21	9.82	133	109.86	121.53	11	12.38	92.52
			Average		67			16	9.62	89.03

 α ρ_1 is the density of pure CO₂ at different experimental pressures and temperatures, which is obtained from the NIST fluid property database.

Table 3

Correlation parameters for the solubility of 3,5-DNBA and m -NBA in SCCO₂ for the binary and ternary systems.

Table 4

Data references for the compounds considered in this study.

Table 5 Correlation parameters for the solubility of compounds in $SCCO₂$ using the modified K–J model.

No.	Compound	D_0	D_1	D_2	D_3
Binary system					
$\mathbf{1}$	5-Sulfosalicylic acid	1.4400e-2	$-1.7089e - 3$	-1730.98	-10.1339
$\sqrt{2}$	p-Aminobenzoic acid	$9.1885e - 3$	$-9.3986e - 4$	-2079.81	-8.0072
3	Ethyl p-hydroxybenzoate	$4.2332e - 2$	$-5.1802e-3$	-4446.84	-1.2031
$\overline{4}$	Ethyl p-aminobenzoate	$5.3548e - 2$	$-6.4727e - 3$	-4138.20	-2.0514
5	p-Toluenesulfonamide	$-3.1718e-3$	7.5725e-4	-3407.34	-0.9067
6	Sulfanilamide	$-4.9720e-3$	$9.6288e - 4$	-4658.22	-1.4730
$\overline{7}$	Benzoic acid	$5.9106e - 2$	$-7.0287e - 3$	-5224.67	0.9408
8	Salicylic acid	$1.0870e - 2$	$-7.8654e - 4$	-5404.26	4.7463
9	Acetylsalicylic acid	$-4.0431e-3$	1.3068e-3	-5947.86	6.2620
10	Medroxyprogesterone acetate	$-4.3570e - 2$	$6.7706e - 3$	-5125.57	5.3012
11	Cyproterone acetate	$-6.2890e - 2$	$9.2829e - 3$	-2611.14	-0.5895
12	Disperse Red 73	$3.2045e - 2$	$-3.8610e - 3$	-4080.03	-3.9635
13	Disperse Yellow 119	$1.8634e - 2$	$-1.8282e-3$	-6815.18	3.0222
Ternary system					
$\mathbf{1}$	5-Sulfosalicylic acid	$1.0395e - 2$	$-1.2122e-3$	-1428.35	-10.4810
	p-Aminobenzoic acid	$1.0750e - 2$	$-1.2635e-3$	-1259.46	-10.1108
2	Ethyl p-hydroxybenzoate	$6.1928e - 2$	$-7.6820e - 3$	-6028.82	2.4032
	Ethyl p-aminobenzoate	$5.7304e - 2$	$-6.9336e - 3$	-4320.61	-1.7311
3	p-Toluenesulfonamide	$-1.1884e - 2$	$2.1132e - 3$	-5480.40	5.0330
	Sulfanilamide	$7.3099e - 3$	$-7.7005e - 4$	-3210.28	-6.3997
$\overline{4}$	Benzoic acid	$4.9411e - 2$	$-5.7279e - 3$	-5143.15	1.4849
	Salicylic acid	$3.1613e - 2$	$-3.3639e - 3$	-5665.65	3.6448
5	Benzoic acid	$3.8320e - 2$	$-4.2100e-3$	-5917.65	4.8504
	Acetylsalicylic acid	$2.7257e - 2$	$-2.5545e-3$	-7178.55	7.1142
6	Salicylic acid	$2.2175e - 2$	$-2.1601e-3$	-5730.32	4.3350
	Acetylsalicylic acid	$-8.9059e - 4$	$1.0116e - 3$	-6546.61	7.7525
$\overline{7}$	Medroxyprogesterone acetate	$-5.4864e - 2$	8.0335e-3	-3744.61	3.5130
	Cyproterone acetate	$-5.9721e-2$	$8.6205e - 3$	-3076.02	1.6648
8	Disperse Red 73	$1.6268e - 2$	$-1.6132e-3$	-4501.55	-2.2870
	Disperse Yellow 119	$4.0710e - 3$	$-8.8115e-5$	-4737.14	0.5843
9	Cholesteryl benzoate	$7.2903e - 2$	$-8.3326e - 3$	-7231.02	0.3612
	cholesteryl butyrate	7.9802e-2	$-9.0984e - 3$	-7724.27	-1.8192
10	Mono-tert-butyl ethers of glycerol	$4.4042e - 2$	$-5.4756e - 3$	-2553.57	-3.2763
	Di-tert-butyl ethers of glycerol	$3.0442e - 2$	$-3.7524e-3$	-1976.88	-4.2448
11	Hexachlorobenzene	$1.1040e - 1$	$-1.4062e - 2$	280.49	-24.4688
	Pentachlorophenol	$3.7362e - 2$	$-4.3201e-3$	-4792.20	0.2005
12	1,10-Decanediol	$-1.8093e-1$	$2.3854e - 2$	-6621.34	30.0567
	Benzoic acid	$5.4004e - 3$	$-9.3819e - 5$	-4289.00	3.9268
13	Phenanthrene	$7.2043e - 2$	$-8.5736e - 3$	-5571.79	-0.6192
	Anthracene	$9.6274e - 2$	$-1.1723e - 2$	-5125.50	-7.4187
Quaternary system					
1	Benzoic acid	$5.2139e - 2$	$-5.9750e - 3$	-5879.24	3.1266
	Salicylic acid	$5.5034e - 2$	$-6.3209e - 3$	-6664.57	4.0592
	Acetylsalicylic acid	$4.9354e - 2$	$-5.3955e-3$	-7475.26	5.7293

where D_0 - D_3 are the model constants, y_2 is the mole fraction solubility of solute in SCF, ρ_1 (g L⁻¹) is the density of pure solvent at different experimental pressures and temperatures, and $T(K)$ is temperature.

3.2. Methodology

The average absolute relative deviation (AARD) of the model from experimental data was calculated according to the following formula:

$$
AARD(\mathscr{E}) = \frac{100}{n} \sum_{1}^{n} \frac{|y_{\text{cal}} - y_{\text{exp}}|}{y_{\text{exp}}}
$$
(6)

where y_{cal} is the calculated value of the mole fraction solubility of solute, y_{exp} is the experimental value of the mole fraction solubility of solute, *n* is the number of experimental points. The name and version of software that we used to fit the experimental and calculated data was Microsoft Office Excel 2007.

4. Results and discussions

For [the](#page-6-0) binary system $(3,5-DNBA/m-NBA + SCCO₂)$ and the ternary system $(3,5-DNBA + m-NBA + SCCO₂)$ (the mass ratio of 3,5-DNBA and m -NBA = 1:1), the mole fraction solubility data of solutes in $SCCO₂$ at 308, 318, and 328 K over the pressures range of 10.0–21.0 MPa are all listed in Table 2. The density of $CO₂$ obtained from the NIST fluid property database is also shown in Table 2. In this work, Chrastil model, the modified Adachi and Lu model, K–J model, and the modified K–J model proposed in our work, Eqs. (2)–(5), were [used to c](#page-3-0)orrelate the solubility data of solids in $SCCO₂$.

4.1. Solubility in the binary system

As shown in Table 2 and Fig. 2, the equilibrium solubility of each solid solute increases with increasing pressure at three temperatures (308, 318, and 328 K). It can attribute to the increase of solvent's density with increasing pressure and the specific stronger interactions between solute and solvent molecules at higher pressure. [The](#page-3-0) [cross](#page-3-0)ove[r](#page-6-0) [pressu](#page-6-0)re regions have been observed, as shown in Fig. 2. They are from 10.5 to 11.2 MPa and 11.2–13.0 MPa for 3,5- DNBA and m-NBA, respectively. The crossover phenomena could be attributed to the competitions between solute's vapor pressure and solvent's density, whose dependences on temperature are in opposite directions. Below the crossover pressure region, the density effect, sensitive to the solute's vapor pressure, is dominant so that the solute is more soluble at low temperature. However, above the **Table 6** Comparison of AARD of the K–J model, modified K–J model and the models discussed from literature.

^a Chrastil is Chrastil model; MST is Méndez-Santiago and Teja model; Bartle is Bartle model; PR-EOS is the Peng–Robinson equation of state.

 b K–J₁ is K–J model.

 K – J_2 is the modified K–J model.

^d The average values of AARD for the binary system.

^e The average values of AARD for the ternary and quaternary systems.

^f The total average values of AARD for all systems.

crossover pressure region, solute's vapor pressure becomes dominant at higher temperature and the density of the solvent turns less sensitive to the solute's vapor pressure. At the crossover point, these two competitive factors effect rather.

The solubility data in Table 2 obtained in this study indicate that 3,5-DNBA has lower solubility in $SCCO₂$ than m -NBA. The difference between 3,5-DNBA and m-NBA is the increase of a nitro-functional group by comparing their molecular structure. Therefore, the centrosymmetric dimmers are present in the crystal of pure 3,5-DNBA [22], which [is](#page-3-0) [the](#page-3-0) [cas](#page-3-0)e in the structures of diversity of m-NBA. Two polymorphic groups make 3,5-DNBA easier to be a potential hydrogen bond acceptor, which indicates that 3,5-DNBA has higher polarity than m -NBA. CO₂ exhibits both non-polar tendencies (low dielectric constant) and 'polar' properties (Lewis acidity, strong quadrupole moment). Due to its structural symmetry, $CO₂$ does not have a dipole moment, but it does have a substantial quadrupole moment that operates over a much shorter distance than dipolar interactions. Although $CO₂$ molecules present a quadrupolar effect, the polarity of $CO₂$ is still smaller than most of polar solvents [23]. Based on the "like-dissolves-like" principle, the more polar a solute, the lower solubility in $CO₂$, the strong polar molecular interaction among the polar 3,5-DNBA molecules impacts on the molecular interaction between 3,5-DNBA and $CO₂$, which le[ads to](#page-9-0) its lower solubility.

In addition, according to the experimental data of the Table 2, at 328 K, the mole solubility of pure m-NBA increases from 1.44×10^{-6} to 109.86 [×] ¹⁰−⁶ significantly; however, the mole solubility of the pure 3,5-DNBA increases from 0.44×10^{-6} to 4.21×10^{-6} . McHugh and Paulaitis illustrated the solubility behavior of a solid in $SCCO₂$ [24]. As they said, A vicinity of upper critica[l](#page-3-0) [end](#page-3-0) [poi](#page-3-0)nt (UCEP) of the binary mixture (m -NBA + SCCO₂) can be reached, which results to the change in solubility with pressure becomes more drastic.

Fig. 2. Experimental solubility data (Table 2) in the binary system in mole fraction (y_b) with pressure (a) 3,5-DNBA + SCCO₂ and (b) m-NBA + SCCO₂ () 308 K; (•) 318 K; (•) 328 K. (a₁ and b₁) The dash lines and solid lines are model correlations based on Chrastil model and the modified Adachi–Lu model, respectively (Eqs. (2) and (3)) and (a₂ and b_2) The dash lines and solid lines are model correlations based on K–J model and the modified K–J model, respectively (Eqs. (4) and (5)) and all the correlation parameters are given in Table 3.

4.2. Solubility in t[he ternar](#page-3-0)y system

The effect of pressure and temperature on the solubility of each [solid](#page-3-0) [s](#page-3-0)olute in the ternary systems follows the same trend as that in the binary systems, as shown in Table 2 and Fig. 3. In the ternary system, the crossover pressure region transferred to 12.0–13.0 MPa for 3,5-DNBA and 12.0–13.5 MPa for m-NBA, respectively.

In order tomake an easier comparison of solubility data between the binary and ternary systems, here the solubility enhancement SE was defined as the [percentag](#page-3-0)e r[elative](#page-7-0) deviation of the ternary solubility from the binary solubility of the component at the same pressure and temperature:

$$
SE(\mathscr{X}) = \frac{y_t - y_b}{y_b} \times 100\tag{7}
$$

where y_b and y_t are the mole fraction solubility of solutes in SCCO₂ in the binary and ternary system, respectively.

The values of SE of these two solutes in the ternary system are listed in Table 2. The average values of SE of 3,5-DNBA at 308, 318, and 328 K are up to 183, 118, and 67, respectively. And the corresponding values of SE of m-NBA are 30, 32, and 16, respectively. Kurnik and Reid [25] have explained the solubility enhancement [in mix](#page-3-0)ed-solid systems in terms of the location of the UCEP. They argued that the higher solubility would be expected in the ternary system at same temperature becaus[e](#page-2-0) [it](#page-2-0) [is](#page-2-0) [close](#page-2-0)r to the UCEP when in comparison to [the](#page-2-0) [binary](#page-2-0) system.

Comparing the values of SE of these two solutes, it indicates that the solubility enhancement of 3,5-DNBA is higher than m-NBA in the ternary system, which were also observed similarly on other solid mixtures [25,26]. The molecular interaction between these two solutes and $CO₂$ may result in the difference. Both 3,5-DNBA and m -NBA have stronger molecular polarity than $CO₂$. Regarding in the ternary system, one solid solute played a "co-solvent" role. Hence two solutes are liable to form the hydrogen bond, which lead[s](#page-9-0) [to](#page-9-0) [the](#page-9-0) [e](#page-9-0)nhancement of their solubility. However, due to the presence of two polar nitro-functional groups, 3,5-DNBA is a relatively stronger proton donor as well as proton acceptor than m-NBA with one nitro-functional group. Therefore, the solubility enhancement of 3,5-DNBA is higher than m -NBA in the ternary system.

4.3. Mixture separation

The effect of operating conditions on selectivity is necessary for the optimal design of a separation process. The appropriate condition for separating these two solids in $SCCO₂$ is confirmed by

Fig. 3. Experimental solubility data (Table 2) in the ternary system (3,5-DNBA + m-NBA + SCCO₂) in mole fraction (y_t) with pressure (a) 3,5-DNBA and (b) m-NBA (■) 308 K; (\bullet) 318 K; (\blacktriangle) 328 K. (a₁ and b₁) The dash lines and solid lines are model correlations based on Chrastil model and the modified Adachi–Lu model, respectively (Eqs. (2) and (3)) and (a₂ and b₂) The dash lines and solid lines are model correlations based on K–J model and the modified K–J model, respectively (Eqs. (4) and (5)) and all the correlation parameters are given in Table 3.

defining the mixt[ure sepa](#page-3-0)ration factor μ and the separation efficiency HE follows:

$$
\mu = \frac{y_{31}}{y_{32}}\tag{8}
$$

$$
HE(\%) = \frac{y_{31}}{y_{31} + y_{32}} \times 100
$$
\n(9)

where y_{31} , y_{32} are the mole fraction solubility of m-NBA and 3,5-DNBA in the ternary system $(3,5-DNBA + m-NBA + SCCO₂)$, respectively.

The separation factor is based upon the assumption that the solute molecules behave independently of each other. As shown in Table 2, the values of mixture separation factor μ range from 3.80 to 12.45. The separation factor μ isotherms of the mixture as a function of experimental pressure at different temperatures are shown in Fig. 4. As can be seen, the separation factor μ enhanced with increasing pressure at three temperatures. In the lower pres[s](#page-3-0)ure region (less than 12 MPa), temperature is not the only factor; however, in the higher pressure region (more than 15 MPa), higher temperature enhanced the separating effect. So in a higher pressure [region](#page-8-0), higher temperature is a positive factor for the separation enhancement in this ternary system.

As shown in Table 2, the average value of HE is proximity to 90, which means that the purity of separation [can](#page-2-0) [be](#page-2-0) advanced to 90%. Thus, it could be ap[plied](#page-2-0) [in](#page-2-0) [th](#page-2-0)e separation of the mixture of 3,5-DNBA and m -NBA using SCCO₂ technology in the industry separ[ation.](#page-3-0)

4.4. Model correlation

The correlated results and optimal parameters of the experimental solubility data using Chrastil model, the modified Adachi and Lu model, K–J model, and the modified K–J model, Eqs. (2)–(5), are listed in Table 3 and shown in Figs. 2 and 3. From Table 3, the solubility data of pure 3,5-DNBA and m -NBA in SCCO₂ are well correlated by all models, Eqs. (2)–(5), with the values of AARD of (3.20–5.03) and (5.10–9.51), respectively. The ex[istence o](#page-2-0)f the UCEP can be the reason why the correlated results of m-NBA with the di[fferent](#page-3-0) [m](#page-3-0)odels are wor[se](#page-6-0) [than](#page-6-0) [that](#page-6-0) [of](#page-6-0) 3,5-DNBA [\[10\].](#page-3-0) Compared with the binary system, for the ternary system, the solubility data of mixed 3,5-DNBA [and](#page-2-0) m -NBA in SCCO₂ are not well correlated by all models, Eqs. (2)–(5), with the values of AARD of (8.54–12.81) and (8.58–12.25), respectively. The molecular interactions in the ternary system are more complicate[d](#page-9-0) [than](#page-9-0) that in the binary

Fig. 4. Separation factor μ (Table 2) isotherms of mixture (3,5-DNBA + m-NBA) in $SCCO₂$ with pressure (\blacksquare) 308 K; (\spadesuit) 318 K; (\spadesuit) 328 K.

system, which may lead to the decline of relations degree and accuracy.

Comparing the values of AARD for all models in Table 3, the modified K–J model proposed in this work (Eq. (5)) correlates the solubility better, which is superior to the existing models, Eqs. (2)–(4). Furthermore, the solubility data of pure and mixed solid solutes in $SCCO₂$ are correlated better by the modified K-J model (Eq. (5)) and the modified Adachi and L[u](#page-3-0) [model](#page-3-0) (Eq. (3)) than Chrastil mo[del](#page-2-0) [\(E](#page-2-0)q. (2)) and K–J model (Eq. (4)). From the expression of models and molecular structures of solid solutes, the reason may result from the complicacy between the solubility of solid solutes and the density of $CO₂(\rho₁)$. Chrastil [and K](#page-2-0)–J models (Eqs. (2) and (4)) illuminate that the relationship between the logarithm of solubi[lity](#page-2-0) [\(](#page-2-0)S or y_2) and the sol[vent](#page-2-0)'s density (ln ρ_1 or ρ_1) is linear. However, the modified K–J and the modified Adachi and Lu models (Eqs. (3) and (5)) indicate the more complicated relationship between the solubility and the solvent's density. Therefore, [t](#page-2-0)he modified K–J and the modified Adachi and Lu models (Eqs. (3) and (5)) are more suitable to correlate the solubility data of solid solutes in $SCCO₂$, especially the modified K–J model (Eq. (5)).

4.5. Verification of the modified K–J model

The solid solubility data of 23 different [solid](#page-2-0) compounds in SCCO2 were collected from literature [27–37], concluding 13 binary systems, 13 ternary systems, and 1 quaternary system. The solubility data were correlated with K–J model and the modified K–J model (Eqs.(4) and (5)). Table 4 shows the experimental conditions of these compounds from literature. The correlated parameters and results are shown in [Tables](#page-9-0) [5](#page-9-0) and 6 along with AARD. It is observed that the new proposed model (Eq. (5)) has successfully correlated the solubility data of all the compounds within 5.11% [AARD.](#page-2-0) [Comp](#page-2-0)[aring](#page-3-0) [wi](#page-3-0)th the correlation result by K–J model (Eq. (4)) with 8.03% AARD, the modified K–J model (Eq. (5)) is superior to K–J model (Eq. [\(4\)\)](#page-4-0) [for](#page-4-0) [corre](#page-4-0)lating the solubility of solid compounds in $SCCO₂$. In addition, as s[how](#page-2-0)n in Table 6, for the binary system, the average AARD of the modified K–J model (Eq. (5)) is 5.26; for the ternary and quaternary systems, the average AARD is 5.04, which indicates that the modified [K–J](#page-2-0) [m](#page-2-0)odel (Eq. (5)) in this study is [able](#page-2-0) to correlate the solubility data of pure and mixed solid compounds with less AARD. Table 6 [also](#page-5-0) [s](#page-5-0)hows the comparison of the AARD obtained by the modified K–J model [\(Eq.](#page-2-0) (5)) and the models from literature. Therefore, the above results indicate the new proposed model (Eq. (5)) presents mor[e](#page-2-0) [acc](#page-2-0)urate correlation

for solubility data of solid compounds in $SCCO₂$, not only for the binary system (pure solute + $SCCO₂$), but also for the ternary system (mixed solutes + $SCCO₂$). It is an excellent practical model that could be employed to speed up the process of SCF applications in the industry.

5. Conclusions

In this work, the solubility of pure 3,5-DNBA and m-NBA and their equal-weight mixture in $SCCO₂$ was determined at 308, 318, and 328 K, over a pressure range from 10.0 to 21.0 MPa. The pressure and temperature effects on solubility in the ternary system were similar to those who obtained in the binary system. The higher polarity of 3,5-DNBA led to its lower solubility in $SCCO₂$ compared with m -NBA both in the binary and ternary systems.

In the ternary system, one solid solute played a "co-solvent" role, which resulted in a significant increase in the solubility of another solute. The effect of solubility enhancement SE has been observed. The average values of SE of 3,5-DNBA at 308, 318, and 328 K are up to 183, 118, and 67, respectively. And the corresponding values of SE of m-NBA are 30, 32, and 16, respectively. The results indicate that the solubility enhancement of 3,5-DNBA is higher than m-NBA in the ternary system. The mixture separation factor μ and the separation efficiency HE were investigated. The maximum values of μ and HE were 12.45 and 92.57, respectively, which indicate it is successful to separate the mixture of $3,5$ -DNBA and m -NBA using SCCO₂ technology.

The modified K–J model was proposed for correlating the solubility of solid compounds in $SCCO₂$. The equilibrium solubility data of pure and mixed solutes in $SCCO₂$ were correlated by Chrastil model, the modified Adachi and Lu model, K–J model, and the modified K–J model with the values of AARD in ranging of (4.75–12.81), (3.20–8.71), (5.03–11.72), and (3.22–8.58), respectively. The modified K–J model proposed in this work correlates the solubility better, which is superior to another three models. Solubility data from 23 different solid compounds were taken from literature and correlated by K–J model and the modified K–J model in good accuracy. The total average values of AARD from K–J model and the modified K–J model were 8.03 and 5.11, respectively.

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